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**Research** Article

# Thermo-Catalytic Methane Decomposition for Hydrogen Production: Effect of Palladium Promoter on Ni-based Catalysts

Irene Lock Sow Mei<sup>1</sup>, S.S.M. Lock<sup>1</sup>, Dai-Viet N. Vo<sup>2</sup>, Bawadi Abdullah<sup>1,3\*</sup>

<sup>1</sup>Chemical Engineering Department, Universiti Teknologi PETRONAS, Bandar Sri Iskandar, 32610, Perak, Malaysia

 <sup>2</sup>Faculty of Chemical & Natural Resources Engineering, Universiti Malaysia Pahang, Lebuhraya Tun Razak, 26300 Gambang, Kuantan, Pahang, Malaysia
 <sup>3</sup>Center of Biofuel and Biochemical Research (CBBR), Universiti Teknologi PETRONAS, 32610, Bandar Seri Iskandar, Perak, Malaysia

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## Abstract

Hydrogen production from the direct thermo-catalytic decomposition of methane is a promising alternative for clean fuel production. However, thermal decomposition of methane can hardly be of any practical and empirical interest in the industry unless highly efficient and effective catalysts, in terms of both catalytic activity and operational lifetime have been developed. In this study, the effect of palladium (Pd) as a promoter onto Ni supported on alumina catalyst has been investigated by using coprecipitation technique. The introduction of Pd promotes better catalytic activity, operational lifetime and thermal stability of the catalyst. As expected, highest methane conversion was achieved at reaction temperature of 800 °C while the bimetallic catalyst (1 wt.% Ni -1 wt.% Pd/Al<sub>2</sub>O<sub>3</sub>) gave the highest methane conversion of 70% over 15 min of time-on-stream (TOS). Interestingly, the introduction of Pd as promoter onto Ni-based catalyst also has a positive effect on the operational lifetime and thermal stability of the catalyst as the methane conversion has improved significantly over 240 min of TOS. Copyright © 2016 BCREC GROUP. All rights reserved

Keywords: Methane cracking; TCD; Metal catalysts; Co-precipitation; Nobel metal

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# 1. Introduction

Hydrogen is one of the most promising and sustainable clean energy sources because the combustion of hydrogen for energy production only produces water and does not contribute to-

Corresponding Author.
E-mail: bawadi\_abdullah@petronas.com.my
(B. Abdullah)
Tel.: +605-3687633, Fax:+605-3654075

wards any greenhouse gases emission to the atmosphere [1]. In addition, the most promising application of hydrogen is for the development of fuel cell, which is a device to convert chemical energy into electricity and heat energy to power automobiles [2]. Hence, extensive research has been performed for the development of cost effective, efficient and safe technology for mass hydrogen production to meet the large global demand for hydrogen.

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Among the hydrogen production technologies, steam methane reforming (SMR) is the most frequently route used to produce hydrogen because the process has high efficiency, low heating value and low operating cost. However, the drawback of using the SMR technology is that it is not environmental-friendly due to the generation of high quantities of greenhouse gases (GHG), which is estimated to be 13.7 kg of  $CO_2$  for every kg of hydrogen produced [3].

The recent discovery that methane can be directly decomposed into hydrogen and carbon nanofibers has drawn the attention for pure hydrogen production through methane thermocatalytic decomposition (TCD) process, also known as the methane catalytic cracking reaction. According to Wang and Lua [4], this process is feasible because it does not produce CO or CO<sub>2</sub> as by-products and do not require watergas shift and additional separation stages to remove CO<sub>2</sub> as compared to the traditional hydrogen production method, which lead to additional economic savings. The carbon produced as by-products during the operation also has advanced properties to be utilized as promising sorbents, catalyst supports and carbonaceous composite materials [4].

Although methane decomposition reaction is an attractive alternative for producing clean energy fuel, it is a moderately endothermic reaction. Non-catalytic decomposition of methane can only happen at extremely high temperature (>1300 °C) to obtain reasonable yield of hydrogen due to the strong C-H bonding within methane. Recently, methane decomposition over catalysts has gained high attention as an alternative route for hydrogen production at lower temperature [5-9]. Among the supported metal catalysts which have been investigated by researchers, Ni-based catalysts have been discovered to be an effective catalytic component for many applications such as dry reforming, steam reforming, TCD and etc. [10]. In particular to the methane cracking process, Nibased catalysts generate promising yield of hydrogen per mass unit of the active component at temperature above 800 °C. However, the hydrogen yield is low (<40 %) due to thermodynamic limitation for hydrogen production at temperature below 800 °C. In addition, another challenge is that the catalyst deactivates very fast due to an encapsulating type of carbon depositing on the active sites of the catalyst [11-14].

The recent study by Srilatha *et al.* [15] has revealed the potential for Pd to increase the catalytic lifetime of catalysts for methane decomposition process. However, the effect of the

addition of Pd onto Ni/Al<sub>2</sub>O<sub>3</sub> catalysts and the properties of the Ni-Pd alloy which is formed is yet to be investigated by researchers. Hence, in this present work, methane decomposition process over 2 wt.% Ni supported on alumina, 2 wt.% Pd supported on alumina, and 1 wt.% Ni 1 wt.% Pd supported on alumina (sample coded as Ni/Al<sub>2</sub>O<sub>3</sub>, Pd/Al<sub>2</sub>O<sub>3</sub> and Ni-Pd/Al<sub>2</sub>O<sub>3</sub>, respectively) was thoroughly studied at 800, 700 and 600 °C, respectively. These catalysts were prepared by co-precipitation technique. The effect of introducing Pd as a promoter on Nickel supported Alumina catalyst and reaction temperature on the catalytic reactivity and lifetime was studied in a fixed bed system for 10 mL/min flow of methane gas. In addition, the synthesized catalyst were characterized by the application of scanning electron microscopy (SEM), Brunauer Emmett and Teller (BET) surface area analysis, X-Ray Diffraction (XRD), Temperature Programmed Reduction (TPR) and Thermogravimetric Analysis (TGA) to compare their morphologies and physico-chemical properties.

#### 2. Materials and Methods

#### 2.1. Materials

The chemicals which are used for the synthesize of the catalysts are aluminum nitrate nonahydrate (98 wt.% purity; Sigma-Aldrich); nickel(II) nitrate hexahydrate (99 wt.% purity; Merck Millipore) and palladium(II) chloride (99 wt.% purity; ReagentPlus) and ammonia solution (5 wt.% purity; Merck Millipore). In addition, highly pure methane gas (99.99 wt.% purity; Sigma-Aldrich) and argon gas (99.88 wt.% purity; Sigma-Aldrich) are used as the reactor influent to evaluate the catalytic activity and performance of the synthesized catalysts.

#### 2.2. Preparation of catalysts

The catalysts were prepared by using the coprecipitation method. The co-precipitation technique involved the homogeneous mixing of nickel, palladium and aluminum precursor solution, and modifying the pH of the solution to precipitate the catalysts out from the mixture by the addition of alkaline solution. Aqueous solution of nickel nitrate hexahvdrate (Ni(NO<sub>3</sub>)<sub>2.6</sub>H<sub>2</sub>O), and palladium(II) chloride (PdCl<sub>2</sub>) were titrated drops by drops into aluminum nitrate nanohydrate (Al(NO<sub>3</sub>)<sub>3</sub>.9H<sub>2</sub>O) solution to enable homogeneous mixing. Next, the mixture was stirred at 60 °C while ammonia solution  $(NH_3, H_2O)$  was added by drop wise to increase the pH of the solution to 10. Then, the solution was heated to 100 °C and the solution was stirred for 1 hour at 300 rpm. The Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst will start to precipitate out of the solution and the slurry was filtered and washed with deionized water to remove excess ammonia solution. This was followed by drying the catalyst overnight in an oven at 100 °C and the calcination of the catalysts at 600 °C for 6 hours with air.

#### 2.3. TCD of methane-catalytic activity testing

The catalytic activity, thermal stability and deactivation rate of the synthesized catalysts were evaluated at atmospheric pressure on a conventional fixed bed gas flow system with 500 mg of catalysts using a single-zone furnace (Carbolite VST 12) without end insulation. The methane decomposition test rig consists of 3 main components, which are the gas mixing system, the fixed bed reactor for methane cracking process to take place and an online gas chromatography system. The test rig for thermo-catalytic methane decomposition reaction is indicated in Figure 1. Before the experimental work is conducted, pure argon gas at 20 mL/min was allowed to flow through the reactor to create an inert atmosphere in the reactor. Next, the co-precipitated catalysts were subjected to reduction pre-treatment with hydrogen gas at 30 mL/min at 600 °C for 1 hour. After reduction, the reactor was flushed with

pure argon gas until the gas chromatography system showed no existence of hydrogen gas.

During the experiment, 10 mL/min of methane gas was diluted with 5 mL/min of argon gas in the gas mixing system before the gas mixture is introduced into the reactor. The flow of methane, hydrogen and argon gas can be regulated by a mass flow controller is located at the inlet stream to the reactor. The temperature of the catalyst bed was measured and monitored by using a thermocouple and temperature controller which is connected directly to the reactor. The reactor effluent is analyzed by using an online gas chromatography system (Hewlett Packard Series 6890) which is located at the outlet of the reactor. The exit stream was analyzed every 15 minutes for a total reaction time of 4 hours and the catalysts were tested at 600, 700, and 800 °C, respectively while the flow rate of methane and gas were maintained at constant value.

For every 15 minutes interval, GC analysis measured the percentage (v/v) composition of the reactor effluent stream and percentage of methane conversion against time were investigated for all the trials. The conversion of methane and the yield of hydrogen are defined and calculated as explained by Mohd Zabidi *et al.* [16].

#### 2.4. Catalyst characterization

The catalysts were analyzed by scanning





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electron microscopy (SEM) to study the surface morphology of the fresh catalysts. The SEM images were taken by using Phillips XL30/FEI ESEM system which was operated at an accelerating voltage from 5 to 30 kV. In addition, the N<sub>2</sub> adsorption-desorption isotherms for the synthesized catalysts were measured on a Micromeritics ASAP 2020 system. All the samples were evacuated at 300 °C in vacuum to remove water and other contaminants prior to the measurement. From N<sub>2</sub> adsorption and desorption isotherms at -196 °C (77 K), the catalysts can be characterized for the determination of the specific surface area and pore volume.

Besides that, powder X-ray diffraction (XRD) spectra were recorded on a Bruker D8 Advance (USA) X-ray diffractometer by using Cu Ka1 radiation ( $\lambda$ =1.54 Å) at 40 kV tube voltage and 40 mA tube current with a scanning speed of 2° per minute between 20° and 80° 2 $\theta$ . The XRD patterns recorded were referenced and compared with the power diffraction database for phase identification.

The reducibility behavior of the catalysts were also investigated by the application of H<sub>2</sub> Temperature Program Reduction technique on a Thermo Finnigan (TPRRO 1100) equipment. Prior to H<sub>2</sub> reduction, the samples were pretreated with nitrogen at 300 °C with a flow rate of 20 mL/min and ramping rate of 10 °C/min and finally holding at 300 °C for 30 minutes to eliminate any impurities. TPR analysis was then conducted in 5% H<sub>2</sub>/N<sub>2</sub> with a flow rate of 20 mL/min. The samples were heated with a ramping rate of 10 °C/min from room temperature to 800 °C and the reduction profile was determined. The catalysts were also characterized by using Thermogravimetric Analysis (TGA) to investigate the weight loss, thermal behavior and structural decomposition of the samples at a heating rate of 10 °C/min up to 800 °C. The weight of the samples were initially at 0.1 g and was performed under sweeping air atmosphere at 10 mL/min.

#### 3. Results and Discussion

#### 3.1. Characterization of calcined catalysts

The Scanning Electron Micrographs at 10,000 magnification are presented in Figure 2. The SEM image of the samples after calcination shows that a porous sponge-like structure, consisting of pyramid-shaped and rod-shaped particles has been formed. However, the particles size are significantly smaller for the Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst and Ni/Al<sub>2</sub>O<sub>3</sub> catalyst than the Pd/Al<sub>2</sub>O<sub>3</sub> catalyst. In addition, the surface areas and pore volumes which were determined by N2 physisorption for the synthesized catalysts are given in Table 1. The adsorption isotherms are indicated in Figure 3. The specific surface areas for the synthesized catalysts varied between 195.31 and 212.80 m<sup>2</sup>/g while the pore volume varied between 0.30 and 0.38 cm3/g. The inhouse prepared Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst demonstrated higher surface area and wider pore volume as compared to the co-precipitated Ni/Al<sub>2</sub>O<sub>3</sub> and Pd/Al<sub>2</sub>O<sub>3</sub> catalysts. The development of high surface area catalysts are significant to achieve high diffusion and mass transfer rate during the methane decomposition process, contributing to higher catalytic activity and reaction rate. In addition, larger pore volumes might be feasible





for rapid molecular transportation, namely higher diffusion efficiency of reactants and products and to avoid the blockage of the active sites of the catalyst due to carbon deposition during the reaction.

The XRD pattern for the calcined Ni/Al<sub>2</sub>O<sub>3</sub>, Pd/Al<sub>2</sub>O<sub>3</sub> and Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalysts are shown in Figure 4. Based on the XRD spectrum for Ni/Al<sub>2</sub>O<sub>3</sub> catalyst, the peak observed at  $2\theta$  = 65.3° corresponded to the formation of defect NiAl<sub>2</sub>O<sub>4</sub> spinel phase. This is because the peak value is detected between the values of  $2\theta$  = 67.3° for  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and  $2\theta = 65^{\circ}$  for stoichiometric NiAl<sub>2</sub>O<sub>4</sub> spinel. The other peaks for the defect NiAl<sub>2</sub>O<sub>4</sub> phase occur at values of approximately  $2\theta = 36^{\circ}$ ,  $45.8^{\circ}$ ,  $59.7^{\circ}$  and  $65.3^{\circ}$ . The peaks observed at  $2\theta = 36^{\circ}$ ,  $45.8^{\circ}$  and  $65.3^{\circ}$  corresponded to the formation of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> lattice while NiO is only detected at the first peak at  $2\theta = 36^{\circ}$ . This may be due to the reason that XRD can typically only detect metal crystallites that are larger than 2-5 nm and NiO crystallite sizes are smaller than the detection limit [17].

In addition, XRD patterns of  $Pd/Al_2O_3$  shows six diffraction peaks. Among these six peaks,

**Table 1.** Surface area and pore volumes forcatalysts

| Type of<br>catalysts              | Surface<br>Area (m²/g) | Pore Volume<br>(cm <sup>3</sup> /g) |  |
|-----------------------------------|------------------------|-------------------------------------|--|
| Ni/Al <sub>2</sub> O <sub>3</sub> | 201.03                 | 0.34                                |  |
| $Pd/Al_2O_3$                      | 195.31                 | 0.30                                |  |
| $Ni-Pd/Al_2O_3$                   | 212.80                 | 0.38                                |  |



**Figure 3.** N<sub>2</sub> adsorption isotherms of catalysts at -196 °C. Symbols represent: (♦) Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst (■) Ni/Al<sub>2</sub>O<sub>3</sub> catalyst and (▲) Pd/Al<sub>2</sub>O<sub>3</sub> cata

Pd peaks appeared at  $2\theta$  angles of  $33^\circ$ ,  $40^\circ$ ,  $45.8^{\circ}$  and  $69^{\circ}$ , while the angles at  $36^{\circ}$ ,  $45.8^{\circ}$ and 65.3°, representing  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> formation. This finding is almost similar to the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> phase observed for co-precipitated Ni/Al<sub>2</sub>O<sub>3</sub> catalyst. Interestingly, the diffraction peak detected at 33° was due to Pd formation in its oxide form (PdO). The XRD spectra suggested the existence of pure Pd<sup>o</sup> along with PdO nanoparticles in the Pd/Al<sub>2</sub>O<sub>3</sub> sample. On the other hand, XRD profile of Ni-Pd/Al<sub>2</sub>O<sub>3</sub> showed eight diffraction peaks with Pd peaks observed at  $2\theta$ angles of 40°, 45° and 69°. The diffraction peaks at  $2\theta = 35.1^{\circ}$ ,  $45^{\circ}$ ,  $48^{\circ}$  and  $63^{\circ}$  corresponded to the formation of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> phase while Ni peaks were detected at 35.1°, 48°, 51°, 60° and 63°. The XRD spectra for the Ni-Pd/Al<sub>2</sub>O<sub>3</sub> sample demonstrated a unique profile which is distinct from that which should be observed from a simple combination of the XRD profiles recorded for the monometallic catalysts. The XRD profile of the sample suggested that alloyed NiPd species has been formed within the catalyst, which is favorable and beneficial for the thermo-catalytic methane decomposition process.

The TPR profiles of the samples are shown in Figure 5 to study the metal-support interaction. For the Ni/Al<sub>2</sub>O<sub>3</sub> catalyst, two zones of reduction peaks are presented. The first zone is observed at the temperature of 400 °C while the second reduction peak is observed at the temperature range between 600 to 700 °C. The reduction peak at lower temperature correspond to the reduction of NiO species which has minimal interaction with the alumina support. The higher temperature reduction peak may be attributed to the strong interaction of spinel NiAl<sub>2</sub>O<sub>4</sub> phase. The formation of a



**Figure 4.** XRD diffractograms of synthesized catalysts. (a) Ni/Al<sub>2</sub>O<sub>3</sub> catalyst, (b) Pd/Al<sub>2</sub>O<sub>3</sub> catalyst and (c) Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst

strong interaction of NiAl<sub>2</sub>O<sub>4</sub> was confirmed by the XRD spectra of Ni/Al<sub>2</sub>O<sub>3</sub> sample and was also reported by other researchers within the temperature range of 550 °C and 750 °C [18-20]. For the  $Pd/Al_2O_3$  catalyst, the TPR traces exhibited a main hydrogen consumption peak due to the reduction of PdO species to metallic palladium. Another reduction peak is observed at 450 °C which could be attributed to Pdalumina support interactions and a strong support de-hydroxylation. The TPR profile was similar to those reported by Garcia et al. [20] for Pd supported on alumina catalysts. On the other hand, the TPR profile of the bimetallic Ni-Pd/Al<sub>2</sub>O<sub>3</sub> is very similar to those corresponding to the monometallic Pd. The Ni-Pd/Al<sub>2</sub>O<sub>3</sub> first peak is at the range of 100 to 200 °C which is due to the reduction of PdO and a second peak at the range of 300 to 600 °C which may be due to the reduction of NiAl<sub>2</sub>O<sub>4</sub> species, which were formed by the diffusion of Ni<sup>2+</sup> into the support. The results is similar to those reported by Lederhos et al. [22]. It can be observed that the presence of nickel shifted the peaks of NiO from 700 °C to lower temperature range, suggesting that the Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst is easier to be reduced.

Figure 6 indicates the relationship between the residual sample weight percentages with the decomposition temperature for all synthesized catalysts. All the samples demonstrated similar TGA traces in which the weight loss increases as the temperature increases. The total weight loss of these co-precipitated catalysts varied within 84 to 86 %. However, the Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst demonstrated higher resistance towards decomposition at high temperature with total weight loss of only 14 % as com-



Figure 5. Temperature-programmed reduction profiles of synthesized catalysts: a) Ni/Al<sub>2</sub>O<sub>3</sub>, (b) Pd/Al<sub>2</sub>O<sub>3</sub> and (c) Ni-Pd/Al<sub>2</sub>O<sub>3</sub>; heating rate of 10 °C/min in 5%  $H_2$  in  $N_2$ 

pared to Ni/Al<sub>2</sub>O<sub>3</sub> (15%) and Pd/Al<sub>2</sub>O<sub>3</sub> (~16%). The finding suggested that the incorporation of Pd onto Ni based catalyst may improve the thermal stability of the catalyst. This finding is significant because the catalyst should be able to have long-term and high thermal stability to prevent the decomposition and deactivation of the catalysts during methane cracking reaction.

# **3.2. Catalytic activity of catalysts for methane decomposition process**

The methane conversion profile for the synthesized catalysts as a function of time for thermo-catalytic methane decomposition within 4 hours on stream at 600, 700, and 800 °C, respectively and the results are shown in Figure 7. The effect of introducing Pd as a promoter to Nickel supported on alumina catalyst were investigated through the experimental work by comparing and evaluating the performance of the synthesized catalysts which can provide high methane conversion with long-term operational lifetime. The experimental results suggested that as the reaction temperature is higher, the catalytic activity also improved significantly. The experimental studies indicated that methane conversion values were the lowest at T = 600 °C for all the synthesized catalysts due to the reduced amount of energy available to break the C-H bonding within methane into hydrogen.

The experimental results also indicates that the methane conversion decreases over time due to carbon deposition on the active sites of the catalysts, resulting in sintering and deactivation of the catalysts during the operation. This results is consistent with the observation



**Figure 6.** Thermo-gravimetric analysis of synthesized catalysts; heating rate of 10 °C/min in sweeping air atmosphere at 10 mL/min

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and findings which were obtained from other studies in which the catalytic activity of the catalysts decrease rapidly within 2 hours on stream even though the initial hydrogen production rate was promising [11, 23-24].

The methane conversion obtained for all the synthesized catalyst within 15 min on stream are summarized in Table 2. The experimental results indicate that when Ni/Al<sub>2</sub>O<sub>3</sub> catalyst is used for the methane cracking process without introducing Pd as a promoter, the methane conversion at 800 °C is at 47%. At 700 °C, the methane conversion is approximately 38% while the methane conversion is only 27% at 600 °C. The methane conversion is the lowest for Pd/Al<sub>2</sub>O<sub>3</sub> catalysts in which the methane conversion is only at 18% at 600 °C and 27% at 700 °C. However, when Pd is introduced as promoter onto the nickel-based catalysts, the methane conversion has improved significantly from 47% to 66% at 800 °C, from 38% to 56% at 700 °C and from 27% to 42% at 600 °C.

The experimental results suggested that the formation of a strong Ni-Pd alloy bonding within the alumina-supported catalysts is beneficial for methane cracking process. This is because the formation of the Ni–Pd bonding increases the catalytic activity of the catalysts,

**Table 2.** Methane conversion within 15 min onstream

which can catalyze a greater number of methane molecules to hydrogen and carbon.

The methane conversion for the synthesized catalysts after they have been used for 240 min on stream are summarized in Table 3. It can be observed that the methane conversion after 4 hours on-stream for Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst are higher than the methane conversion which is obtained for the monometallic supported on alumina catalyst. This is attributed to the presence of Pd within the structure of the catalysts, which has enhanced the thermal stability of the catalyst at elevated temperature by reducing the tendency for deactivation due to coking and sintering. The co-precipitated Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst remained active (conversion> 20%) although it has been used on-stream for 4 hours. This maybe due to the higher surface area and homogeneous morphology of the catalyst resulted in an improved capability of the catalyst to accumulate carbon, thus contributing towards higher operational lifetime of the catalysts by making it less susceptible to deactivation and coking. In addition, the uniform dispersion of Ni and Pd particles which can be observed from the SEM images enables higher interaction between the catalyst and methane to take place, even when some of the active

**Table 3.** Methane conversion within 240 min onstream

|   | C       | Conversion (%) |        | Cataluat                             | Conversion (%)  |        |                      |  |
|---|---------|----------------|--------|--------------------------------------|---|--------|----------------------|--|
| Catalyst600 °C  |         | 700 °C         | 800 °C | Catalyst                             | 600 °C  | 700 °C | 800 °C               |  |
| Ni/Al <sub>2</sub> O <sub>3</sub>   | 27.41   | 37.91          | 47.12  | Ni/Al <sub>2</sub> O <sub>3</sub>    | 6.03  | 11.24  | 15.33                |  |
| $Pd/Al_2O_2$  | 18 23   | 22.89          | 35.61  | Pd/Al <sub>2</sub> O <sub>3</sub>    | 5.59  | 10.23  | 15.68                |  |
| Ni-Pd/Al <sub>2</sub> O <sub>3</sub>                                      | 42.18   | <b>56.82</b>   | 66.88  | Ni-Pd/Al <sub>2</sub> O <sub>3</sub> | 15.55   | 20.31  | 24.56                |  |
| Wethane Conversion (%)<br>0 0 0<br>0 0<br>0 0<br>0 0<br>0 0<br>0 0<br>0 0 | 120 180 | 240            |        | 120 180 2                            | 050<br>040<br>05<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 |        | <b>*************</b> |  |
| Time (Min)  |         |                |        | Time (Min)                           |   |        |                      |  |
|   | (a)     |                |        | (b)                                  |   | (c)    |                      |  |

**Figure 7.** Percentage of methane conversion against time at (a) 800 °C, (b) 700 °C and (c) 600 °C. Symbols represent: (♦)Ni-Pd/Al<sub>2</sub>O<sub>3</sub> catalyst (■) Ni/Al<sub>2</sub>O<sub>3</sub> catalyst and (▲) Pd/Al<sub>2</sub>O<sub>3</sub> catalyst

sites of the catalyst has been blocked by carbon particles.

#### 4. Conclusions

The results of the study suggested that the addition of Pd on Ni/Al<sub>2</sub>O<sub>3</sub> catalysts for the thermo-catalytic methane decomposition has a significant effect on the catalytic activity and thermal stability of the catalyst at high temperature. The 2% Ni/Al<sub>2</sub>O<sub>3</sub> catalyst without Pd loading rapidly deactivated due to the formation of condensed encapsulating carbon during the methane cracking process which can block the activation sites of the catalyst. On the other 1%Ni-1%Pd/Al<sub>2</sub>O<sub>3</sub> was hand, the stable throughout the methane decomposition process with a lower deactivation rate. The finding suggested that an increase in stability at elevated temperature is attributed to the addition of Pd as a promoter onto the surface of the coprecipitated catalyst. The interaction of Pd particles with the metallic Ni particles resulted in an enhanced ability to suppress carbon formation, thus increasing the catalytic lifetime of the catalyst.

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#### References

- Abbas, H., Wan Daud, W. (2010). Hydrogen Production by Methane Decomposition: A Review. International Journal of Hydrogen Energy, 35: 1160-1190.
- [2] Lesmana, D., Wu, H. S. (2012). Short Review: Cu Catalyst for Autothermal Reforming Methanol for Hydrogen Production. Bulletin of Chemical Reaction Engineering & Catalysis, 7: 27-42.
- [3] Wu, H., Parola, V., Pantaleo, G., Puleo, F. (2013). Ni-based Catalysts for Low Temperature Methane Steam Reforming: Recent Results on Ni-Au and Comparison with Other Bi-metallic Systems. *Catalysts*, 3: 563-583.
- [4] Wang, H., Lua, A. (2013). Hydrogen Production by Thermocatalytic Methane Decomposition. *Heat Transfer Engineering*, 34(11-12): 896-903.
- [5] Awadallah, A., Mostafa, M., Aboul-Enein, A., Hanafi, S. (2014). Hydrogen Production via

Methane Decomposition over Al<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub> Binary Oxides Supported Ni Catalysts: Effect of Ti Content on The Catalytic Efficiency. *Fuel*, 129: 68-77.

- [6] Zhou, L., Guo, Y., Hideo, K. (2014). Unsupported Nickel Catalysts for Methane Catalytic Decomposition into Pure Hydrogen. *AICHE Journal*, 60(8): 2907-2917
- [7] Jin, L., Si, H., Zhang, J., Lin, P., Hu, Z., Qiu, B. (2013). Preparation of Activated Carbon Supported Fe-Al<sub>2</sub>O<sub>3</sub> and Its Application for Hydrogen Production by Catalytic Methane Decomposition. *International Journal of Hydrogen Energy*, 38(25): 10373-10380.
- [8] Ahmed, S. (2013). Catalytic Decomposition of Methane for Hydrogen Production Using Different Types of Catalysts. *Titrit Journal of Engineering Science*, 20(5): 19-23.
- [9] Wang, G., Jin, Y., Liu, G., Li, Y. (2013). Production of Hydrogen and Nanocarbon from Catalytic Decomposition of Methane over A Ni-Fe/Al<sub>2</sub>O<sub>3</sub> Catalyst. *Energy and Fuels*, 27 (8): 4448-4456.
- [10] Selvarajah, K., Nguyen, H.H.P., Abdullah, B. Alenazey, F., Vo, D-V.N. (2016). Syngas production from methane dry reforming over Ni/Al<sub>2</sub>O<sub>3</sub> catalyst. *Res. Chem. Intermed*, 42(1): 269-288, doi: 10.1007/s11164-015-2395-5
- [11] Adrian, L., Abella, L.C., Monroy, T.G. (2014). Hydrogen Production via Thermo Catalytic Decomposition of Methane over Bimetallic Ni-Cu/AC Catalysts: Effect of Copper Loading and Reaction Temperature. *International Journal of Chemical Engineering and Application*, 3(2): 92-97.
- [12] Amin, A., Epling, W., Croiset, E. (2011). Reaction and Deactivation Rates of Methane Catalytic Cracking over Nickel. *Industrial & Engineering Chemistry Research*, 50: 12460-12470.
- [13] Makvandi, S., Alavi, S. M. (2011). CO<sub>x</sub> Free Hydrogen Production by Catalytic Decomposition of Methane over Porous Ni/Al<sub>2</sub>O<sub>3</sub> Catalysts. *Iranian Journal of Chemical Engineering*, 8(4): 24-33.
- [14] Bai, Z., Chen, H., Li, B, Li. W (2007). Methane Decomposition over Ni loaded Activated Carbon for Hydrogen Production and the Formation of Filamentous Carbon. *International Journal of Hydrogen Energy*, 32(1): 32-37.
- [15] Srilatha, K., Srinivasulu, D., Ramakrishna, S.U.B., Himabindu, V. (2014). Thermo Catalytic Decomposition of Methane over Pd/AC and Pd/CB Catalysts for Hydrogen Production and Carbon Nanofibers Formation. International Journal of Engineering Research and Applications, 4(9): 81-86.
- [16] Shah, N., Panjala, D., Huffman, G.P. (2001). Hydrogen production by catalytic decomposi-

# Bulletin of Chemical Reaction Engineering & Catalysis, 11 (2), 2016, 199

tion of methane. Energy Fuels, 15(6): 1528-1534.

- [17] Poncelet, G., Centeno, M., Molina, R. (2005). Characterization of reduced α-aluminasupported nickel catalysts by spectroscopic chemisorption measurement. Applied Catalysis A: General, 288: 232-242.
- [18] Yaakob, Z., Bshish, A., Ebshish, A., Tasirin, S.M., Alhasan, F. H. (2013). Hydrogen Production by Steam Reforming of Ethanol over Nickel Catalysts Supported on Sol Gel Made Alumina: Influence of Calcination Temperature on Supports. *Journal of Materials*, 6: 2229-2239.
- [19] Zhang, X., Liu, J., Jing, Y., Xie, Y. (2003). Support Effects on the Catalytic Behavior of NiO/Al<sub>2</sub>O<sub>3</sub> for Oxidative Dehydrogenation of Ethane to Ethylene. *Applied Catalysis A: General*, 240: 143-150.
- [20] Negrier, F., Marceau, E., Che, M., de Caro, D. (2003). Role of Ethylenediamine in the Prepartion of Alumina-Supported Ni Catalysts from [Ni(en)<sub>2</sub>(H<sub>2</sub>O)<sub>2</sub>](NO<sub>3</sub>)<sub>2</sub>: From Solution Properties to Nickel Particles. Comptes Resdus Chimie, 6: 231-240.

- [21] Garcia, G., Vargas, J. R., Valenzuela, M.A., Rebollar, M., Acosta, D. (1999). Palladium Supported on Alumina Catalysts Prepared by MOCVD and Impregnation Method. *Materi*als Research Society, 549: 237.
- [22] Lederhos, C. R., Badano, J.M., Quiroga, M. E., L'Argentiere, P.C., Coloma-Pascual, F. (2010). Influence of Ni Addition to a Low-Loaded Palladium Catalysts on the Selective Hydrogenation of 1-Heptyne. *Quimica Nova*, 33(4): 18-28.
- [23] Uddin, M., Wan Daud, W., Abbas, H. (2014). Co-production of hydrogen and carbon nanofibers from methane decomposition over zeolite Y supported Ni catalysts. *Energy Conversion* and Management, 90: 218-229.
- [24] Al-Hassani, A., Abbas, H., Wan Daud, W. (2014). Production of COx-free hydrogen by thermal decomposition of methane over activated carbon: Catalyst deactivation. *International Journal of Hydrogen Energy*, 39(27): 14783-14791.

Selected and Revised Papers from The International Conference on Fluids and Chemical Engineering (FluidsChE 2015) (http://fluidsche.ump.edu.my/index.php/en/) (Malaysia, 25-27 November 2015) after Peer-reviewed by Scientific Committee of FluidsChE 2015 and Reviewers of BCREC